

Research Article

## Development of low formaldehyde emitting particle board by nano particle reinforcement

### Ranjana Yadav

Department of Chemistry, Indian Plywood Industries Research & Training Institute, Centre, Mohali -160055 (Punjab), India

Email: ranjanay7@gmail.com

### Article Info

<https://doi.org/10.31018/jans.v13i4.2959>

Received: August 28, 2021

Revised: October 20, 2021

Accepted: October 26, 2021

### How to Cite

Yadav, R. (2021). Development of low formaldehyde emitting particle board by nano particle reinforcement. *Journal of Applied and Natural Science*, 13(4), 1187 - 1197. <https://doi.org/10.31018/jans.v13i4.2959>

### Abstract

Nanoscience and nanotechnology offer a plethora of possibilities for improving the qualities of wood composites. The present study aimed to use nanotechnology to develop low formaldehyde emitting particle board as ecologically acceptable composites. Conventional urea Formaldehyde resins were prepared by the percentage of second urea at 10%. Nano-wollastonite, silica and montmorillonite with the size range of 25-100 nm were applied at 0.5-2.0% based on the weight of resin. The nano-reinforced resins were admixed with suitable hardener and the panels were made. Formaldehyde emission reduction in wood panel products is critical and it can be partially controlled by using resin modification. The effectiveness of nanoparticle addition to reducing formaldehyde emission from wood particle board was examined by the perforator method as per IS 13745 (1993). Physical and Mechanical properties were evaluated according to IS 3087 (2005). The result indicated distinctly lower water absorption and thickness swelling of panels produced with 1.5 %, 1.5 % and 2.0 % nano silica, nano montmorillonite and nano wollastonite respectively. The results showed that static bending of the produced composite varied from 21.07 to 28.86 N/mm<sup>2</sup> of MOR and from 2246 - 3353 N/mm<sup>2</sup> of MOE; while internal bond strength (IB) varied from 0.35 to 0.58 N/mm<sup>2</sup>. As per IS 3087 (2005) requirements, 1.5 % nano silica and montmorillonite and 2.0 % nano wollastonite mechanically modified urea formaldehyde based agro composites gave the best results for grade II particle boards. The study concluded that nanoparticle addition reduces the formaldehyde content in the panel without affecting the strength properties.

**Keywords:** Nanoparticle, Particle board, Urea formaldehyde resin, Mechanical properties

## INTRODUCTION

The wood panel industry depends on polycondensed thermosetting resins, of which urea formaldehyde is one of the most significant (Ciraci, 2005; and Lei *et al.*, 2008). Particle board panels are created from wood particles and are a renewable bio resource. Particle board panels are commonly used in furniture and decoration, whereas plywood panels are mostly employed for structural purposes (Azambuja *et al.* 2018; Hameed *et al.* 2019; Hernández *et al.* 2020; Iždinský *et al.* 2020, Farah *et al.* 2021)

Formaldehyde emission is an important feature to consider when purchasing wood panels for home usage. Formaldehyde has a recognised harmful effect on human health (Roffael, 2006; Salthammer *et al.*, 2010 and Anonymous, 2012). Wood composite panels emit formaldehyde as a result of their formaldehyde-based resin content, which is a disadvantage in many

applications. The current glue industry's principal goal is to meet both of these needs by developing effective urea formaldehyde resin with very low, if not nil, formaldehyde emissions. Cademartori *et al.*, (2019) added small percentages of aluminium oxide nanoparticles into UF resin and investigated thermo-mechanical properties of the composites. They reported that aluminium oxide nanoparticles were effective to reduce the formaldehyde emission (14%) from MDF based on the results of the desiccator test. pMDI may be regarded as the most obvious formaldehyde-free adhesive candidate (Solt *et al.* 2019).

For wood composite materials, nanoscience and nanotechnology offer several benefits. The use of nanotechnology in the production of particle board panels is critical in addressing the formaldehyde emission problem (Johnes *et al.*, 2005; and Roughley, 2005). Throughout the last two decades, nanotechnology has been used

to improve the properties of a variety of materials, including solid wood and wood composite panels (Dukarska, 2013; Gallo *et al.*, 2013; Hassani *et al.*, 2019; Esmailpour *et al.*, 2019; and Esmailpour *et al.*, 2020). Large particles of the same substance appear to cause a series of distinct material characteristics changes that nanoparticles do not (Li, 2012). A green binder was developed with oxidized corn-starch (OCS) and urea (U) for wood-based panel production. Nano-TiO<sub>2</sub> modified the obtained adhesive. Developed OCS – U based adhesive can be used with traditional melamine urea formaldehyde resin as a hybrid adhesive system for producing particleboards with low formaldehyde content (Oktay *et al.* 2021).

Nanomaterials contain a lot of mechanical qualities and unique properties that aren't seen in micromaterials. Thus they have a lot of future potentials (Haghighi-Poshtiri, 2013; Taghiyari, 2013 a; Taghiyari and Nouri, 2015; Taghiyari *et al.*, 2016a; Taghiyari *et al.*, 2016b; Taghiyari *et al.*, 2018; and Reinprecht *et al.* 2018). Valle *et al.* (2021) studied the influence of SiO<sub>2</sub> nanoparticles on the physical and mechanical properties of wood particleboard. They showed that panels produced with the nanoparticles 42% reduction in thickness swelling of the panel.

However, more research into nanomaterials is required. To find potential technical applications and industrial productions, we must first establish the mechanical properties of distinct nanomaterials. Some natural scavengers such as chestnut shell flour, phenolated kraft lignins, tannins extractives, soy flour (Taghiyari *et al.* 2020), melamine, polyvinyl alcohol, and adipic acid dihydrazide (Liu *et al.* 2020), alizarin red sulfonate, alizarin yellow-GG, and chromotropic acid decreased the formaldehyde emission from wood-based panels produced with UF resin (Kord *et al.* 2021). There is only limited research on the formaldehyde emissions of particle board enhanced with nanomaterials under various settings (Moubarik *et al.*, 2010; Candan and Akbulut, 2012; Taghiyari *et al.*, 2013; Taghiyari *et al.*, 2013b;

Karmi *et al.*, 2013; Candan and Akbulut, 2015; Poshitri 2015; Waheed *et al.* 2020). The study aimed to create an environmentally friendly particle board with minimal formaldehyde emissions and to investigate the impact of nanoparticle loading on thermosetting resins.

## MATERIALS AND METHODS

### Materials

*Poplar* particles were taken from our headoffice IPIRTI, Bangalore. Industrial grade urea and formaldehyde were purchased from Oswal Scientific Pvt. Ltd, Chandigarh. Wollastonite (Kemolite KFB-1010) was provided by M/s Wolkem India Limited, Rajasthan, India, for project work as a free sample. Silica and montmorillonite was purchased from Sigma Aldrich.

### Methodology:

#### Preparation of nanoparticle

Commercially obtained wollastonite (KFB-1010), silica and montmorillonite (K10) powder particles with an average particle size of about 8 µm, 0.03 µm, around 6-13µm respectively were used as starting materials. Properties of bulk particles are given in Table 1. A high-energy planetary ball mill machine was used for ball milling (Retsch PM 100). Zirconium balls with a diameter of 10 mm were confined in a bowl as the milling container. Hardened chromium steels were used to make both the ball and the bowl. The ball to powder weight ratio was preserved at 4:1 in all runs, and the bowl rotation speed was around 300 rpm. The speed was selected as per instrument and materials. Milling was done in an open environment at ambient temperature (Fig.1). XRD was used to determine the structure of the samples. This software was used for calculating the crystallite size and internal strain of the sample by the following equation (Williamson and Hall, 1953).

$$d = \frac{K \times \lambda}{\beta \times \cos \theta} \quad \text{-----Eq. 1}$$

**Table 1.** Properties of bulk particles

S.N.	Properties	Wollastonite (Kemolite KFB-1010)	Silica	Montmorillonite (K10)
1	Chemical properties(%)	Metasilicate 94.78 CaSiO <sub>3</sub> (CaO+ SiO <sub>2</sub> ) 0.78 R <sub>2</sub> O <sub>3</sub> (Fe <sub>2</sub> O <sub>3</sub> + Al <sub>2</sub> O <sub>3</sub> )	Silicon= 46.83 Oxygen=53.3	Phylosilcate SiO <sub>2</sub> =43.77 Al <sub>2</sub> O <sub>3</sub> =18 CaO=1.02 Na <sub>2</sub> O=1.03 H <sub>2</sub> O=35.6
2	Physical properties			
	Brightness	85.10	-	-
	Density	490kg/m <sup>3</sup>	02.3lb/cu.ft	300-370kg/m <sup>3</sup>
	Particle size	3.88µm	0.2-0.3 µm	6-13µm
	Moisture content	0.04%	-	-



Fig. 1. Preparation of nano particles.

$$\epsilon = \beta / 4 \tan \theta \quad \text{-----Eq. 2}$$

Where  $\theta$  is the Bragg diffraction angle,  $d$  is the crystallite size,  $\epsilon$  is the average internal strain,  $\lambda$  is the wavelength of the radiation used,  $\beta$  is structural broadening, which is the difference in integral profite width between the standard and sample, and  $K$  is the Scherrer Constant (0.89-0.91). Intergral width gives an evaluation that is independent of the distribution in size and shape. Peak width is defined by integral breadth.  $K$  can vary with the morphology of the crystalline domains.

### Synthesis of urea-formaldehyde resin

Conventional urea-formaldehyde resin was employed with a molar ratio of urea-formaldehyde of 1:2 (mole ratio or weight ratio of urea formaldehyde= 1:2) for the manufacturing of particle board. To ensure complete synthesis of methyl urea, the reactants are allowed to react at pH 8.0 for 2 hours at  $90 \pm 2^\circ\text{C}$  under reflex. The reaction was then completed by adding taces of dilute acetic acid (4.5-5) leading to the formation of urea-formaldehyde polymer. The pH was adjusted to 7.5-8 and the remaining urea was added to reduce the formaldehyde concentration when the desired viscosity is achieved (flow time in B4 flow cup 20-25 sec at ambient temperature). After then, the resin was allowed to cool to ambient temperature.

The requirement for adding second urea was to keep a specified quantity of free urea in the resin system to mop up free formaldehyde that may be present at the conclusion of the preparation and to mop up free formaldehyde generated during particle board hot pressing. All attempts to add second urea to the particle board resulted in the removal of a significant amount of free formaldehyde. Table 2 lists the qualities of resin.

Table 2. Properties of resin

S.N.	Properties	UF
1	Flow time of Resin in B4 flow cup (Sec)	20-22
2	Gelation time at $100^\circ\text{C}$ (sec)	73
3	pH of the resin	8.25
4	Solid content (%)	50.53
5	Water tolerance	1:3-4

### Method of adhesive mixing

A known weight of wood particles was obtained. Three-layer particle boards were made with 8% solid resin on the weight of oven-dried core particles and 12% solid resin on the weight of face particles. Resin was mixed with various percentages of micro particles (0.5-2.0%). The dispersion of nanoparticles in the Urea-formaldehyde resin was done by mechanical mixing. The resin was admixed with the required quantity of hardener on the basis of the solid content of resin. The adhesive was slowly added to the wood particles and mixed uniform so as to distribute the adhesive to all the particles. During mixing resin with the particles, the entire quantity of particle was taken in a tray and the resin was slowly poured on the particles. The resin may be added batch-wise and mixing continued by hand. The process of mixing by hand is continued until uniform mixed material is obtained. The adhesive formulation for manufacturing particle board is given in Table 3. The resin quantity was calculated as per literature (Razali *et al.*, 2012).

### Mat formation

In the present case, mat formation was done manually. Various stages of mat formation are shown in Fig 2.

**Table 3.** Adhesive formulation for particle board

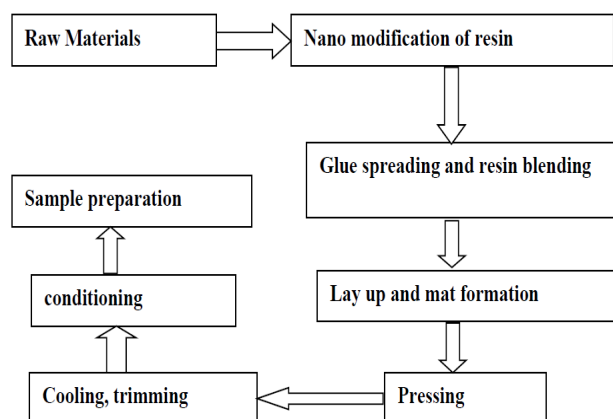
S.N.	Particulars	Resin	
		Face	Core
1	Particles	320 gm	480 gm
2	Resin required	85 gm	85 gm
3	Nano particles (wollastonite, Silica and montomorilonite)	0.5-2.0% of resin	0.5-2.0% of resin
4	Wax Emulsion 1%	0.85 gm	0.85 gm
5	Scavenger 2%	1.7 gm	1.7 gm
6	Liq Ammonia	1 ml	1 ml
7	Hardener water mixed with hardener	0.34 gm 2.52 gm	0.51 gm 2 gm

Three mm thick aluminium caul plates of required board dimension with 10 % excess in margin was taken. A square wooden frame with dimensions equal to that of the aluminium caul plates. BOPP paper was placed over the aluminium caul plate, followed by the wooden frame. Glued particles are taken inside the frame and spread uniformly by hand. The lid is placed over the particles within the frame and pressed hard to compact the particles, as far as possible. By keeping the lid in place, the frame was removed slowly without affecting the mat. The lid is then removed. A BOPP paper was placed over the mat and finally covered with a aluminium caul plate. Aluminium rods of required thickness (thickness of the board to be made) were placed on two-sided of the furnish formed mat. The assembly was ready for hot pressing. The pre-pressed mat assembly was then inserted into a 350 mm X 350 mm hot press, where the platens were kept at a temperature of 160 to 50 degrees Celsius. Supporting rods to control the thickness to 12 mm were placed on either end of the assembly. A pressure of 25 kg/cm<sup>2</sup> for compression cycle for 6 minutes both the resin system followed by curing cycle of 12 kg/cm<sup>2</sup> for about 6 minutes curing time was employed for 12 mm thick particle board.

The pressure was initially increased to get a high surface density on the board. After the time was up, the pressure was reduced to zero for a few seconds to release the steam that had built up on the boards, and the final result was taken from the hot press. After being removed, the boards were piled on a level platform to achieve moisture equilibrium before being trimmed to size. Fig. 2 shows the end output of particle composites.

**Method for the determination of Formaldehyde Emission Content**

The formaldehyde content emission was determined by Perforator method as per IS 13745:1993 “Method for determination of formaldehyde content is particle board by extraction method” (Table 5). The method involved boiling the specimen in toluene, collecting the driven off



**Fig. 2.** Particle board manufacturing process.

formaldehyde in water, and analysing it using the Iodometric method. The formaldehyde content/ emitted is obtained by the formula given:

$$= \frac{3.0 (V_0 - V_1) (100 + H)}{M} \dots\dots\dots \text{Eq. 3}$$

= 'x' mg/100 gm of oven dry board

V<sub>0</sub> is the consumption in ml of 0.010 mol/l thiosulphate solution for the blank test

V<sub>1</sub> is the consumption in ml of 0.010 mol/l thiosulphate solution for the test

H is the moisture content of the particle board in %

M is the mass in grams of test pieces before the extraction.

**RESULTS AND DISCUSSION**

Fig.3-8 represents the XRD pattern of wollastonite, silica and montomorilonite powder particles before and after milling. Figures reported the 2 theta angle spectrum 10-70<sup>0</sup> angle range. Based on the XRD pattern, the main peak of 2θ positioned at 30<sup>0</sup>, 25.8<sup>0</sup> and 21.6<sup>0</sup> correspond to lattice planes (320), (101), (001) of each ∞ and β of nanowollastonite, nano silica and nano montomorillonite. The XRD patterns of bulk particles showed a very sharp diffraction peak of pure crystalline micro powder. After milling processes, peaks are broadening and decrease in their intensities were observed.

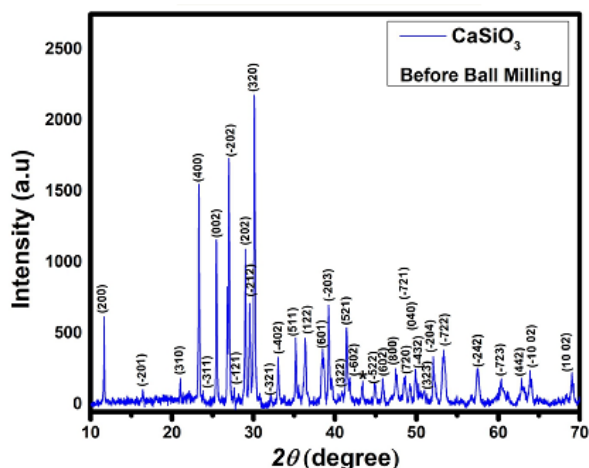


Fig. 3. XRD image of Bulk wollastonite.

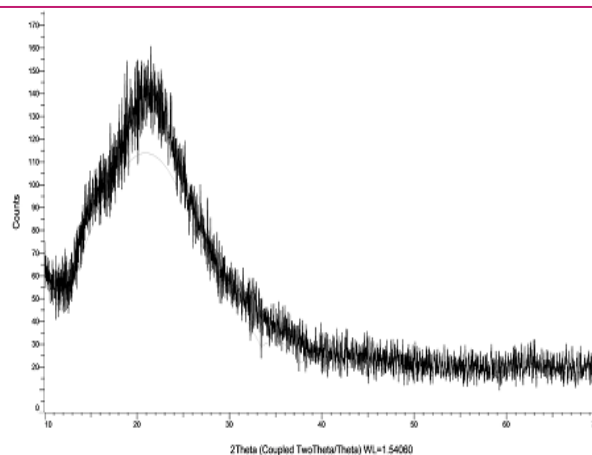


Fig. 4. XRD image of Bulk SiO<sub>2</sub>.

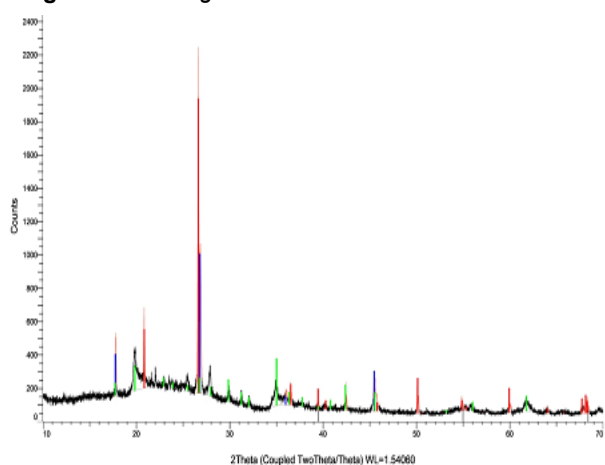


Fig.5. XRD image of Bulk K10.

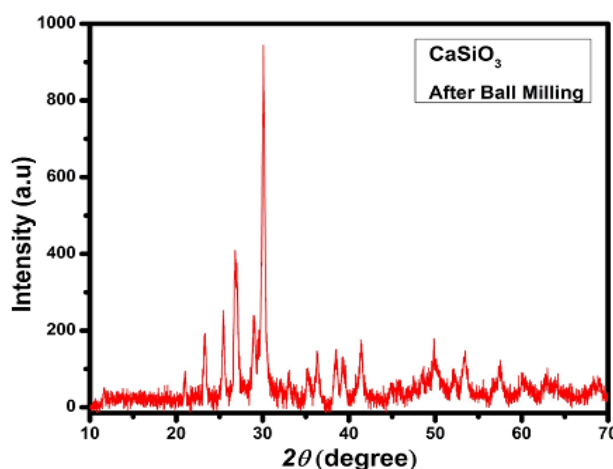


Fig. 6. XRD image of nano wollastonite.

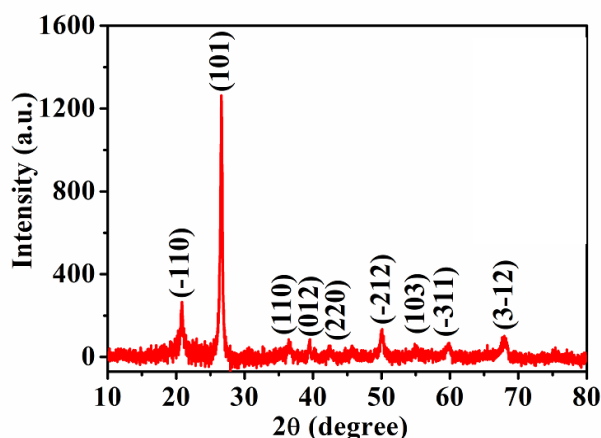


Fig. 7. XRD image of nano SiO<sub>2</sub>.

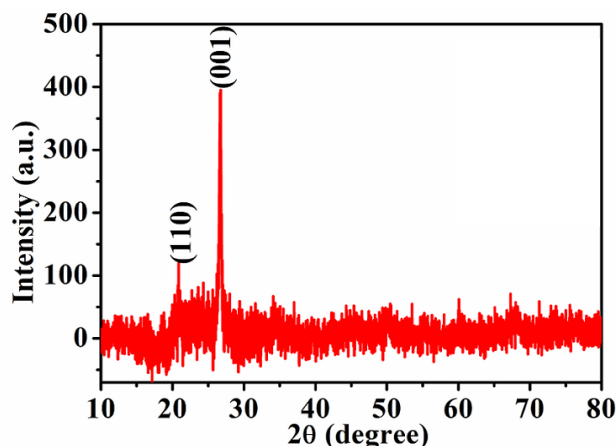


Fig. 8. XRD image of nano K10.

This phenomenon (a broadening of the peaks and a reduction in their intensities) was typical of material after milling and was usually related to the existence of small crystalline particles and internal stresses generated by mechanical impacts. Peak broadening could be caused by both a reduction in crystallite size and an increase in lattice strain, as is well known. During ball

milling in a planetary ball mill, initial powder particles suffer from very strong high energy impacts attributed to collisions between the ball themselves and the container wall. Large amounts of microstructural and structural changes will occur in the milled powder particles as a result of these powerful impacts. Crystallite size refinement and increased lattice strain result from the

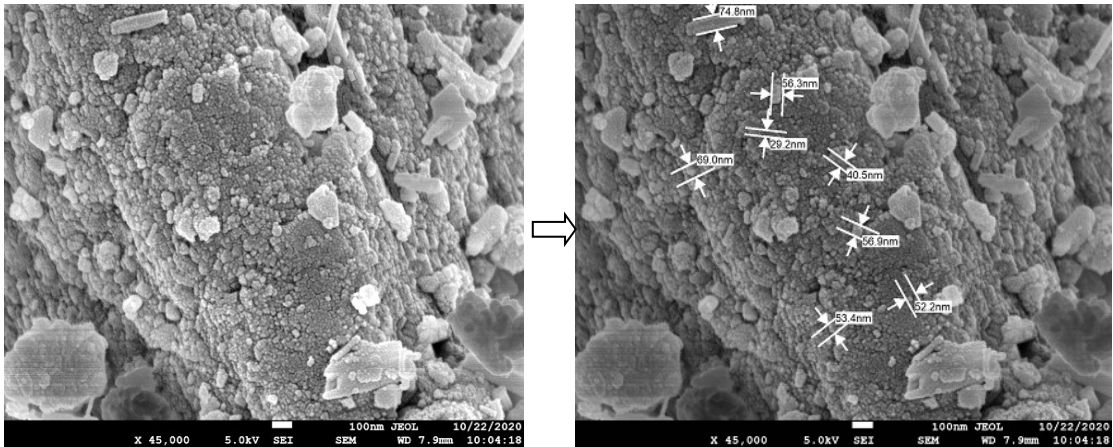


Fig. 9. FESEM micrographs of nano wollastonite.

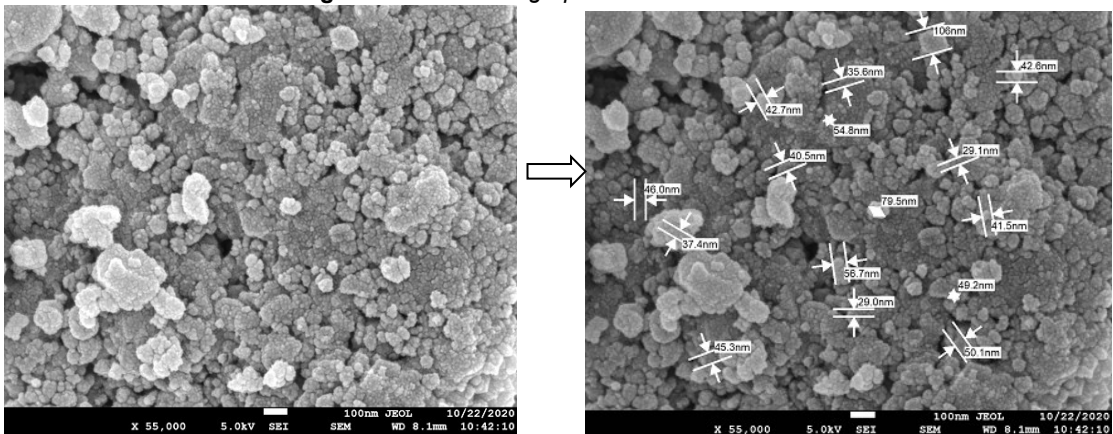


Fig. 10. FESEM micrographs of nano SiO<sub>2</sub>.

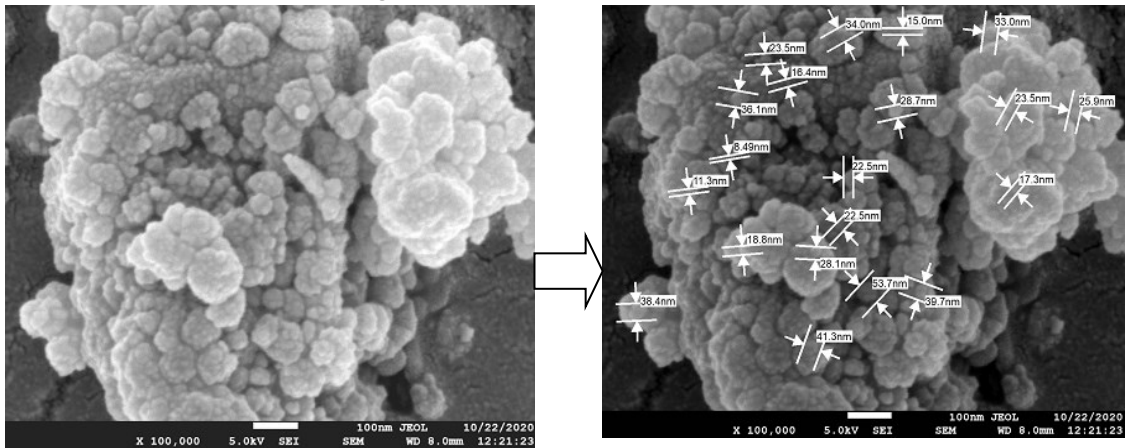


Fig. 11. FESEM micrographs of nano K10.

gradual accumulation of faults and their interaction. For the manufacture of nano particle powder particles, the high energy ball milling technique was a very efficient, practically easy, and low-cost process.

**Field Emission Scanning Electron Microscope (FESEM)**

FESEM was used to view the sample surface. The analysis was done by Central Instrument facility, LPU, Jalandhar. The samples were gold-coated to ensure that the electron beam had sufficient conductivity. Figs.

9-11 show typical FESEM pictures of milled powder. The average particle size of powder particles was around 8 m, 0.03 m, 6-13 m wollastonite, silica, and K10, respectively. The average particle size of nano particles was detected in the range of 25-100 nm in different magnifications when considering the morphologies of the powders milled (Fig. 9-11). The size of particle in SEM micrographs was determined with the help of image analyser software by LPU, shown in Figs. 9-11. The produced nanoparticles were uneven in shape and size, as evidenced by SEM micrographs. Nanopar-

**Table 4.** Physical and mechanical properties of Particle board

S.No.	Properties	Prescribed value as per IS 3087-(2005) Grade-2	Control UF Resin	Physical and Mechanical Properties											
				WO <sub>0.5</sub>	WO <sub>1.0</sub>	WO <sub>1.5</sub>	WO <sub>2.0</sub>	Sl <sub>0.5</sub>	Sl <sub>1.0</sub>	Sl <sub>1.5</sub>	Sl <sub>2.0</sub>	K <sub>0.5</sub>	K <sub>1.0</sub>	K <sub>1.5</sub>	K <sub>2.0</sub>
1.	Density, Kg/m <sup>3</sup>	500-900	723	758.7	772.5	774	759.4	752	774	783	756	755	763	774	755
2.	Moisture content, %	5 – 15	9.7	5.94	5.89	5.79	5.86	5.97	6.32	6.42	6.28	6.8	6.59	6.76	6.80
3.	Water Absorption, %														
	After 2 hours of soaking	Max 40	32.7	31.9	30.76	28.56	26.43	29.86	26.53	23.6	28.1	30.7	29.76	24.8	26.75
3.	After 24 hours of soaking	Max 80	61.8	69.96	65.4	62.8	54.7	61.3	59.7	52.8	59.5	64.5	61.75	54.6	58.79
	Swelling due to general absorption, %														
4.	(After 2 hours soaking)	Max 12	6.2	6.86	5.35	4.98	4.86	6.5	5.15	4.65	5.02	6.58	5.55	4.89	5.61
	a) Thickness	Max 0.5	0.29	0.3	0.29	0.26	0.24	0.28	0.26	0.21	0.24	0.32	0.28	0.23	0.25
	b) Width	Max 0.5	0.29	0.29	0.28	0.24	0.22	0.27	0.26	0.19	0.22	0.30	0.27	0.21	0.24
5.	Modulus of rupture, N/mm <sup>2</sup>														
	Average	Min. 11	24.5	21.07	24.79	24.46	28.75	22.6	26.7	28.5	21.62	24.7	24.72	28.86	26.56
5.	Min. Individual	Min 10	21.6	19.34	23.85	23.76	28.38	21.45	24.61	25.1	18.63	23.9	25.01	26.39	23.48
										7		5			
6.	Modulus of elasticity, N/mm <sup>2</sup>														
	a) Average	Min. 2000	3353	2246	2298	2465	2589	2400	2580	2930	2890	2365	2700	2860	2780
6.	b) Min. Individual	Min 1800	3078	2178	2193	2393	2496	2190	2514	2723	2709	1970	2159	2654	2374
	Tensile strength perpendicular to surface (IB strength), N/mm <sup>2</sup>														
7.	Swelling in thickness due to Surface Absorption (after 2 hours soaking), %	Min 0.3	0.35	0.36	0.43	0.47	0.52	0.43	0.48	0.56	0.52	0.39	0.48	0.58	0.43
	Screw withdrawal strength, N	Max 9	7.6	4.9	3.8	2.06	1.99	4.76	3.95	1.98	2.24	5.1	3.76	2.15	2.56
9.	Face	Min 1250	1680	2100	2245	2875	2950	2375	2590	3086	2976	2285	2456	2986	2860
	Edge	Min 700	876	915	1071	1471	1860	1286	1480	1905	1876	1121	1425	1891	1786

ticles in the sample had a semi-spherical shape. Particle board panels were cut to size and evaluated for the physical and mechanical properties as per IS 3087 (Table 4).

#### **Water absorption and thickness in swelling**

Although particle board panels are commonly utilised in interior applications, they must nonetheless resist water absorption. According to visual inspection, there was no visual difference between the control panels and the panels with nano particle content. When nanoparticles were up to 1.5 percent in the mat in the case of SiO<sub>2</sub> and K10, and 2 percent in the case of wollastonite, water absorption decreased significantly; however, when nanoparticle content was more than this, water absorption increased. The explanation for this can be traced back to the density of different treatments being equal. After 2 and 24 hours, water absorption in nano particle treated panels was lower than in control panels.

Table 4 shows the thickness in swelling values for the nanoparticle panel and the control panel. The results show that the nano material loading amount, nano material type, and the combined effect of these factors considerably reduced the thickness swelling values of the composites after all water soaking periods. The nano particles were used in the composites in this work at a 0.5-2 percent loading level. It was clear that a smaller nano particle loading level had a beneficial effect on thickness swelling properties, whereas a higher loading level had a negative effect. The amount of water that infiltrated through the spaces between particles and the number of swollen fibres was found to have a good association, suggesting a link between the amount of water that infiltrated through the particles and the number of swollen fibres.

#### **Modulus of Rupture (MOR), Modulus of Elasticity (MOE) and Internal Bond (IB) strength properties:**

Table 4 shows the results on the mechanical properties of the board as a function of the amount of nano particle added to the urea-formaldehyde resin. As shown in the results, adding a small amount of nanoscopic wollastonite, silica, and K10 to the glue resin (in the range of 0.5-2 percent) generated a considerable increase in the board IB in comparison to the control board. When the amount of nano particle was increased, the IB dropped to a level that was comparable to the control board. The increased wood adhesive contact and removal of gaps on the wood surface by nano particles can be linked to an increase in nano-reinforced boards' bonding strength.

In addition, adding a small amount of nano to a glue resin improved the boards' bending strength MOR and MOE. Table 4 shows the modulus of rupture and modulus of elasticity of the nano reinforced and control boards. All of the nano composites had greater MOR

values than the control panel. The MOR of the nano panels increased as the nano material loading level increased from 0.5-1.5 percent Nano SiO<sub>2</sub> and K10 to 2% Wollastonite. The maximum MOR value was found in 1.5 percent reinforced composites.

The modulus of elasticity values of the composites reinforced with nano particles increased as the nanomaterial loading level increased up to 1.5 percent in Nano SiO<sub>2</sub> and K10 and up to 2 percent in Wollastonite, whereas the modulus of elasticity values fell. The reason for increasing mechanical properties due to increasing the crosslink density of urea-formaldehyde resin. Further, the mechanical properties of particles boards depend on the bond between particles and adhesive and the quality of the particles. The bonding of particles- adhesive can be improved by increasing the contact surface area between the matrix and particles.

#### **Formaldehyde emission content**

Nanomaterials have distinct properties, such as high chemical activity, physical characteristics as well as a big specific surface area. These characteristics could be leveraged to improve the performance of thermosetting resins and composite materials, opening up new possibilities. Some nanoparticles, however, are prone to aggregation in liquid. Increased nano particle loading levels may have generated aggregation in the nano reinforced resins, lowering the formaldehyde emission value. The particle board panels were made using urea-formaldehyde that had been changed with different nano particles at varying loading levels.

Table 5 shows the formaldehyde data for the nanomaterial reinforced particle board panels and the control panels. UF nanocomposites could effectively decrease the formaldehyde emission of the UF adhesive. The emission was reduced after adding up to 1.5 percent nano Silica and K10 and 2 % wollastonite to the adhesive formaldehyde. However, increasing the level of nano particle loading resulted in more formaldehyde emission. The reason is as follows: firstly, nano particles could adsorb the formaldehyde; secondly, crosslinking network of the UF nanocomposites could prevent the formaldehyde from escaping from the polymer and thirdly, structural stability of the network became stronger and the polymer chain; could not easily be broken to emit formaldehyde (Danyliuk et al. 2020 ). It could be noted that the formaldehyde emission was least when the nanosilica and nano K10-1.5% and wollastonite 2.0% were used. The reason for that particles was dispersed in the solution. When the content was high, it was more difficult for the particles to be dispersed in the solution (Cademartori et al. 2019; Song et al., 2021). The active group of urea-formaldehyde can react with a group available in nano particle (Lin et al., 2006; Roumeli et al., 2012).



**Table 5.** Formaldehyde content in the panels

S.No	Nano Particle percentage	Sample Code	Formaldehyde content in mg/100 gm of dry board
1.	UF Resin	UF	8.9
2.	Wollastonite (KFB-1010)		
(i)	0.5	WO <sub>0.5</sub>	6.85
(ii)	1.0	WO <sub>1.0</sub>	5.63
(iii)	1.5	WO <sub>1.5</sub>	4.86
(iv)	2.0	WO <sub>2.0</sub>	3.2
3.	Silica Powder		
(i)	0.5	SI <sub>0.5</sub>	6.1
(ii)	1.0	SI <sub>1.0</sub>	4.05
(iii)	1.5	SI <sub>1.5</sub>	2.15
(iv)	2.0	SI <sub>2.0</sub>	3.82
4.	Montomorillonite (K10)		
(i)	0.5	K <sub>0.5</sub>	5.9
(ii)	1.0	K <sub>1.0</sub>	4.25
(iii)	1.5	K <sub>1.5</sub>	2.48
(iv)	2.0	K <sub>2.0</sub>	3.9

## Conclusion

Converting micronized particles into nano form by mechanical milling with planetary ball mill is a simple and effective method. The use of nanoparticles for UF resin results in significant decrease of formaldehyde release from the produced particle boards. NanoSiO<sub>2</sub>, nano montomorillonite, and nano wollastonite were used to reinforce particleboard composites at different loading levels i.e. 0.5-2.0 %. Peaks broadening and decrease in their intensities were observed in nanoparticle XRD image. The average particle size of nanoparticles was detected in the range of 25-100 nm by FESEM.

It was found that the fortification of UF resin with 1.5 % nano silica and nano montomorillonite and 2 % nanowollastonite can be considered as an optimum level. Results showed that optimum level have significantly lower water absorption, thickness swelling, low formaldehyde emission and higher mechanical strength. The density of the prepared particle board was achieved between 750-800 kg/m<sup>3</sup> for dimensions of 0.3 X 0.3 X 0.012 mm. As for modulus of rupture and modulus of elasticity, the highest performance was obtained in the composites reinforced with 1.5 % nano silica and nano montomorillonite and 2 % nanowollastonite. The study found that nanoparticle (1.5 % nano silica and nano montomorillonite and 2 % nanowollastonite) reduced the formaldehyde content in the panel without affecting the strength properties. Thus, it would help in developing low formaldehyde emitting environmentally friendly wood composite panels by nanoparticle modified resin.

## ACKNOWLEDGEMENTS

This work has been done under the institute project (funded by MOEF&CC, GOI) with the permission of Director, IPIRTI, Bangalore. I would like to special

thanks to Mrs. Menaka Jha, Scientist, Institute of Science & Technology, Mohali for converting micro particles to nano particles and XRD analysis.

## Conflict of interest

The author declare that she has no conflict of interest.

## REFERENCES

- Anonymous (2012). National Cancer Institute, Formaldehyde and cancer risk. <http://www.cancer.gov/canertopics/factsheet/Risk/formaldehyde>.
- Azambuja, R. R., Castro, V. G., Trianoski, R. & Iwakiri, S. (2018). Recycling wood waste from construction and demolition to produce particleboards. *Maderas Cienc. Technol.*, 20, 681–690. <http://dx.doi.org/10.4067/S0718-221X2018005041401>.
- Cademartori, P. H. G., Artner, M. A., De Freitas, R. A., Esteves Magalhães, W. L. (2019). Alumina nanoparticles as formaldehyde scavenger for urea-formaldehyde resin: Rheological and in-situ cure performance. *Compos. Part B: Engg.*, 176, 107281-107290. <https://doi.org/10.1016/j.compositesb.2019.107281>.
- Candan, Z. & Akbulut, T. (2012). Developing environmentally friendly wood composites panels by nanotechnology. *Bioresources*, 8 (3), 3590-3598. <http://dx.doi.org/10.15376/biores.8.3.3590-3598>
- Candan, Z. & Akbulut, T. (2015). Physical and mechanical of nanoreinforced particle board composites. *Maderas. Ciencia Y Tecnologia*, 17 (2), 319-334. <http://dx.doi.org/10.4067/S0718-221X2015005000030>.
- Ciraci, S. (2005). Science and technology at one of a billionth of a meter. Science and Technology, Tubitak, Ankara, Turkey.
- Danyliuk, N., Tomaszewska, J. & Tatarchuk, T. (2020) Halloysite nanotubes and halloysite-based composites for environmental and biomedical applications. *J. Mol. Liq.*, 309, 113077. <https://doi.org/10.1016/j.arabjc.2021.10.32.94>.
- Dukarska, D. (2013). The effect of an addition of nano SiO<sub>2</sub> to urea resin on the properties of boards manufac-

- tured from rape straw. *Forestry and Wood Technology*, 82, 242-245.
9. Esmailpour, A., Taghiyari, H. R., Majidi, R., Morrel, J. J. & Mohammad-Panah, B. (2021). Nano-wollastonite to improve fire retardancy in medium-density fiberboard (MDF) made from wood fibers and camel-thorn. *Wood Material Science & Engineering*, 16, 161-165. <https://doi.org/10.1080/17480272.2019.1641838>.
  10. Esmailpour, A., Taghiyari, H. R., Ghorbanali, M. & Mantains, G. I. (2020). Improving fire retardancy of Medium density fibre board by nano wollastonite. *Fire and materials*, 1, 8. <http://dx.doi.org/10.1002/fam.2855>.
  11. Farah, A. N. I., Zaidon, A., Anwar, U. M. K., Rabiatal-Adawiah, M. A. & Lee, S. H. (2021). Improved performance of wood polymer nanocomposite impregnated with metal oxide nanoparticle-reinforced phenol formaldehyde resin. *J. Tropical Forest Sci.*, 33, 77-87.
  12. Gallo, E., Schartel, B., Acierno, D., Cimino, F. & Russo, P. (2013). Tailoring the flame retardant and mechanical performances of natural fiber-reinforced biopolymer by multi-component laminate. *Composites Part B: Engineering*, 44 (1), 112-119. <http://dx.doi.org/10.1016/j.compositesb.2012.07.005>.
  13. Haghighi-Poshtiri, A., Taghiyari, H. R. & Karimi, A. N. (2013). The optimum level of nano-wollastonite consumption as fire retardant in poplar wood (*populous nigra*). *Int. J. Nano dimension*, 42 (2), 141-151. <http://dx.doi.org/10.7508/IJND.2013.02.007>.
  14. Hameed, M., Rönnols, E. & Bramryd, T. (2019). Particleboard based on wood waste material bonded by leftover cakes of rape oil. Part 1: The mechanical and physical properties of particleboard. *Holztechnologie*, 6, 31-39. <http://dx.doi.org/10.3390/f11111166>.
  15. Hassani, V., Taghiyari, H. R., Schmidt, O., Maleki, S. & Papadopoulos, A. N. (2019). Mechanical and physical properties of Oriented Strand Lumber (OSL): The effect of fortification level of nanowollastonite on UF resin. *Polymer*, 11, 1884. <https://doi.org/10.3390/polym11111884>.
  16. Hernández, D., Fernández-Puratich, H., Cataldo, F. & González, J. (2020) Particle boards made with *Prunus avium* fruit waste, *Case Studies in Construction Materials* 12, e0033. <https://doi.org/10.1016/j.cscm.2020.e00336>.
  17. IS 13745 (1993) Method for determination of formaldehyde content in particle board by extraction method called perforator method.
  18. Iždinský, J., Vidholdová, Z. & Reinprecht, L. (2020). Particleboards from Recycled Wood. *Forests*, 11, 1166. <https://doi.org/10.3390/f11111166>.
  19. Jones, P., Wegner, T., Atella, R., Beecher, J., Caron, R., Catchmark, J., Koukoulas, A., Lancaster, P., Perine, L., Rodriguiz, A., Ragauskas, A. & Zhu, J. (2005). Nanotechnology for the forest product industry-Vision and technology roadmap, Report based on Nanotechnology for the forest products industry workshop, Landsdowne, Virginia, USA, October 17-19, 2005, TAPPI Press, Atlanta, GA, USA.
  20. Karimi, A., Taghiyari, H. R., Fattahi, A., Karimi, S., Ebrahimi, A. H. & Tarmian, A. (2013). Effect of wollastonite nanofibers on biological durability of poplar wood (*Populus nigra*) against *Trametes Versicolor*. *Bioresources*, 8 (3), 4134-4140.
  21. Kord, B., Farnaz, M., Laleh, A. N. A. (2021). Decreasing Formaldehyde Emission from Particleboard Panels Fabricated by Adding Newly Phenolic Compounds as a Scavenger to Urea Formaldehyde Resin. <http://dx.doi.org/10.21203/rs.3.rs-560970/v1>.
  22. Lei, H., Du, G., Pizzi, A. & Celzard, A. (2008). Influence of nanoclay on urea formaldehyde and phenol formaldehyde resins for wood adhesives. *Journal of Adhesion Science & Technology*, 109, 2442-2451. <http://dx.doi.org/10.1002/app.28359>.
  23. Li, D. (2012). Nanostructuring materials towards conventionally unachievable combination of desired properties. *Journal of Nanomaterials & Molecular Nanotechnology*, 1 (1), 3. <http://dx.doi.org/10.4172/2324-8777.1000e102>.
  24. Lin, Q., Yang, G., Liu, J. & Rao, J. (2006). Property of nano-SiO<sub>2</sub>/urea formaldehyde resin. *Front. For. China* 2,230-237.
  25. Liu, K., Su, C., Ma, W., Li, H., Zeng, Z. & Li, L. (2020). Free formaldehyde reduction in urea-formaldehyde resin adhesive: Modifier addition effect and physicochemical property characterization. *BioRes.*, 15, 2339- 2355.
  26. Moubarik, A., Allai, A., Pizzi, A., Charrier, F. & Charrier, B. (2010). Preparation and mechanical characterization of particle board made from maritime pine and glued with bio adhesives based based on cornstarch and tannis. *Maderas. Ciencia Y Tecnologia*, 12 (3), 189-197. <http://dx.doi.org/10.4067/S0718-221X2010000300004>.
  27. Oktay, S., Nilgün, K. & Basak, B. (2021). Oxidized cornstarch – Urea wood adhesive for interior particleboard production. *Int. J. Adhesion & Adhesives*, 110, 102947. <https://doi.org/10.1016/j.ijadhadh.2021.102947>.
  28. Poshtril, H. R. (2015). The optimum level of nano wollastonite consumption in particle board. *J. Mechanical Engg. Research & Develop.*, 37 (1), 11-21. <http://dx.doi.org/10.7508/IJND.2013.02.007>.
  29. Razali, N. S., Hazan, N. A. M. & Noh, I. A. (2012). Manufacturing of particle board from oil palm frond, Final year project report, Diploma in wood industry, faculty of applied science- Universiti Teknologi MARA.
  30. Reinprecht, L., Iždinský, J. & Vidholdová, Z. (2018). Biological resistance and application properties of particleboards containing nano-zinc oxide. *Adv. Mater. Sci. Eng.*, 2018, 1-8. <http://dx.doi.org/10.1155/2018/2680121>.
  31. Roffael, E. (2006). Volatile organic compounds and formaldehyde in nature, wood and wood based panels. *Holz als Roh- und Werkstoff*, 64, 144-149. <https://doi.org/10.1007/s00107-005-0061-0>.
  32. Roughley, D. J. (2005). Nanotechnology: Implications for the wood product industry. Final Report, Forintek Canada Corporation, North Vancouver, Canada, 73.
  33. Roumeli, E., Papadopoulou, E., Pavlidou, E., Vourlias, G., Bikiaris, D., Paraskevopoulos, K. M. & Chrissafis, K. (2012). Synthesis, Characterization and Thermal analysis of urea formaldehyde/ nanoSiO<sub>2</sub> resins. *Thermochimica Acta*, 527, 33-39. <http://dx.doi.org/10.1016/j.tca.2011.10.007>.
  34. Salthammer, T., Mentese, S. & Marutzky, R. (2010). Formaldehyde in the door environment. *Chemical Review*, 110, 2536-2572. <http://dx.doi.org/10.1021/cr800399g>.
  35. Solt, P., Johannes, K., Wolfgang, G. A., Wolfgang, K., Johann, M., Roland, M., Hendrikus, W. G. van Herwijnen. (2019). Technological performance of formaldehyde free adhesive alternatives for particle board industry. *Int. J.*

- Adhesions & Adhesives*, 94,99-131. <https://doi.org/10.1016/j.jjadhadh.2019.04.007>.
36. Song, J., Chen, S., Yi, X., Zhao, X., Zhang, J., Liu, X. and Liu, B. (2021). Preparation and Properties of the Urea-Formaldehyde Res-In/Reactive Halloysite Nanocomposites Adhesive with Low-Formaldehyde Emission and Good Water Resistance. *Polymers*, 13, 2224. <https://doi.org/10.3390/polym13142224>.
37. Taghiyari, H. R., Mohammad-Panah, B. & Morrell, J. J. (2016a). Effects of wollastonite on the properties of medium-density fiberboard (MDF) made from wood fibers and camel-thorn. *Maderas. Ciencia Y Tecnologia*, 18 (1), 157-166. <http://dx.doi.org/10.4067/S0718-221X201600500016>.
38. Taghiyari, H. R., Majidi, R. & Jahangiri, A. (2016b). Adsorption of nanowollastonite on cellulose surface: effects on physical and mechanical properties of medium-density fiberboard (MDF). *CERNE*, 22 (2), 215-222. <http://dx.doi.org/10.1590/0104776020162222146>.
39. Taghiyari, H. R., Ghamsari, F. A. & Salimifard, E. (2018). Effects of adding nano-wollastonite, date palm prunings and two types of resins on the physical and mechanical properties of medium-density fibreboard (MDF) made from wood fibres. *Bois et Forêts des Tropiques*, 335, 49-57. <http://dx.doi.org/10.19182/bft2018.335.a31517>.
40. Taghiyari, H. R., Karimi, A. & Tahir, P. M. D. (2013). Nano-wollastonite in particleboard: Physical and mechanical properties. *BioResources*, 8(4), 5721-5732.
41. Taghiyari, H. R. & Nouri, P. (2015). Effect of nano wollastonite on physical and mechanical properties of medium density fibre board. *Maderas. Ciencia Y Tecnologia*, 17 (4), 8. <http://dx.doi.org/10.4067/S0718-221X201500500072>.
42. Taghiyari, H. R., Rangavar, H. & Nouri, P. (2013 a). Fire retarding properties of nano wollastonite in MDF. *European Journal of Wood and Wood Products*, 71 (5), 573-581. <http://dx.doi.org/10.1007/s00107-013-0711-6>.
43. Taghiyari, H. R., Mobini, K., Samodi, Y. S., Doosti, Z., Karime, F., Asghari, M., Jahangiri, A. & Nouri, P. (2013b). Effect of wollastonite nanofibers on the improvement of thermal conductivity coefficient of Medium-Density Fiberboard (MDF). *Journal of Nano Materials & Molecular Technology*, 2.1. <http://dx.doi.org/10.4172/2324-8777.1000106>.
44. Taghiyari, H. R., Hosseini, S. B., Ghahri, S., Ghofrani, M. & Papadopoulos, A. N. (2020) Formaldehyde emission in micron-sized wollastonite-treated plywood bonded with soy flour and urea-formaldehyde resin. *Appl. Sci.*, 10, 6709-6723. <https://doi.org/10.3390/app10196709>.
45. Valle Ana, C. M., Bruno, S. F., Glauca, A. P., Danielle, G. & Cristiane I. de C. (2020). Physical and mechanical properties of particleboard from *eucalyptus grandis* produced by urea formaldehyde resin with  $SiO_2$  nanoparticles. *Engenharia Agrícola, Jaboticabal*, 40, 289-293. <http://dx.doi.org/10.1590/1809-4430-Eng.Agric.v40n3p289-293/2020>.
46. Waheed, G., Hussein, A., Shah, S. R. A. & Khan, A. (2020). Effect of Iron Oxide Nanoparticles on the Physical Properties of Medium Density Fiberboard. *Polymers*, 12, 2911. <https://doi.org/10.3390/polym13030371>.
47. Williamson, G. K. & Hall, W. H. (1953). X-ray line broadening from filed aluminium and wolfram. *Acta Metallurgica*, 1, 22-31. [https://doi.org/10.1016/0001-6160\(53\)90006-6](https://doi.org/10.1016/0001-6160(53)90006-6).